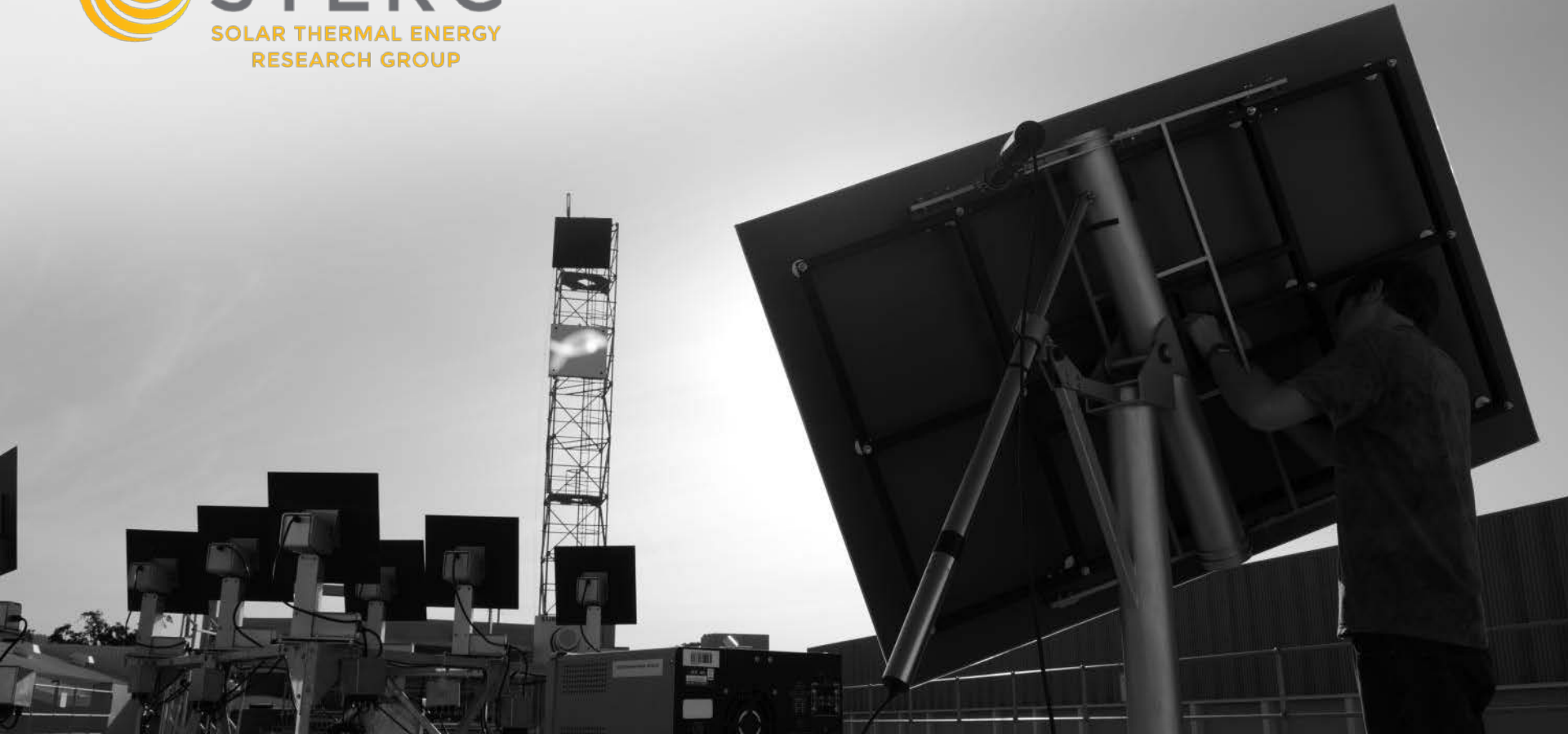




STERG

SOLAR THERMAL ENERGY
RESEARCH GROUP



Design and Testing of Externally Finned Tube Cavity Receiver for Brayton Cycle Preheating Purposes

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Overview



The experimental research process undertaken

- Background of research
- Methodology employed
- Results and observations
- Conclusions

Air as HTF for CSP cycles



Why air?

- Freely available
- Safe, stability at high temperatures
- Absence of phase change
- No risk of freezing
- Brayton cycle integration

SUNDISC cycle



Stellenbosch University Direct Storage Charging Dual-Pressure Air Receiver

- Co-generation power cycle
- Aimed at bypassing the Bottleneck of GT

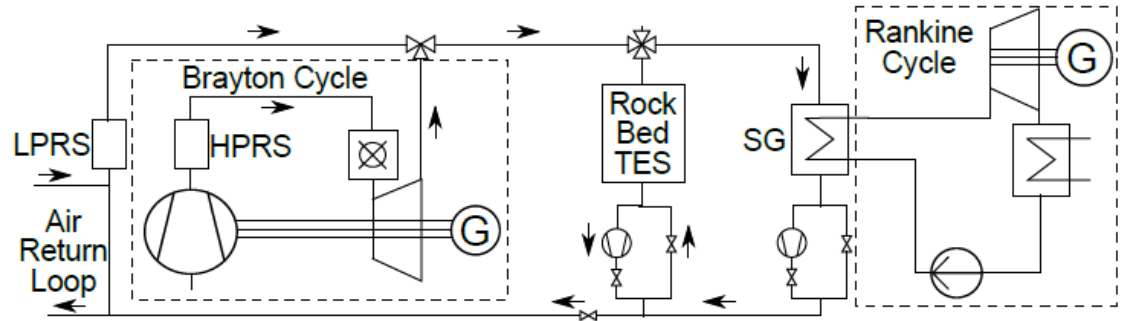


Figure 1: Schematic of the SUNDISC cycle (Heller,2016)

The modified HPAR



Hybrid Pressurised Air Receiver

- Tubular volumetric cavity design
- Pressurised internal air
- Induced flow into the cavity
- Macro and micro cavity effects

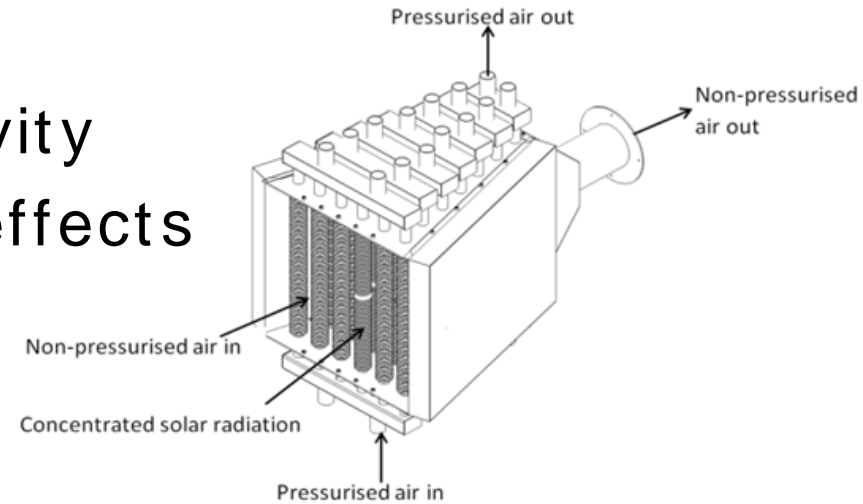


Figure 2: Schematic of the HPAR

Receiver design



Process overview

- Literature
- Simulation

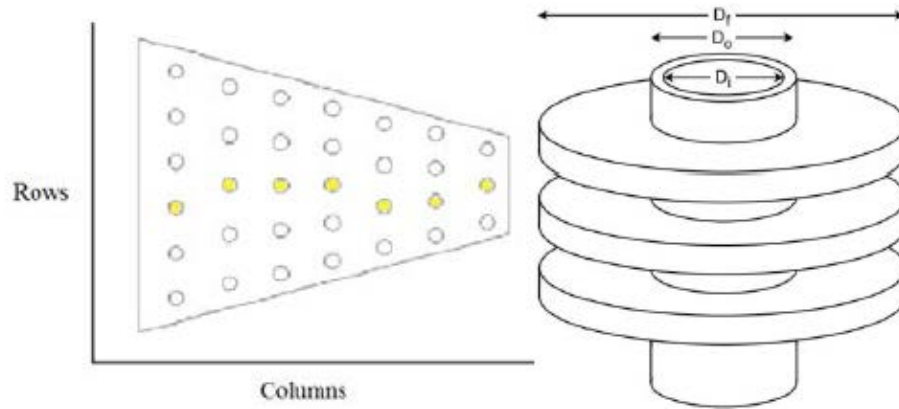


Figure 3: Cavity and tube layout

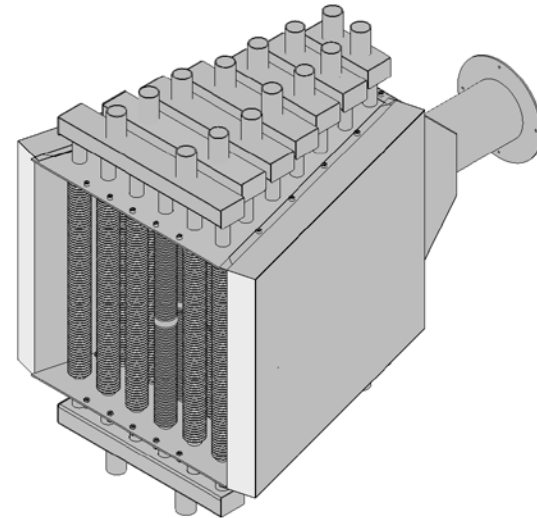


Figure 4: Final test receiver

Construction and installation



Process undertaken



Figure 5: Machining of the fins



Figure 6: Instrumenting the receiver

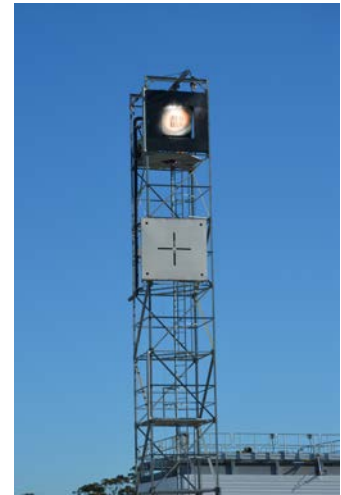


Figure 7: Installed on the tower

Experimental testing overview



34:45 hours of testing

- Half and full heliostat field
- Windless and windy days
- Isolated both the internal and external fluid
- Variation in both the internal and external fluid mass flow rate

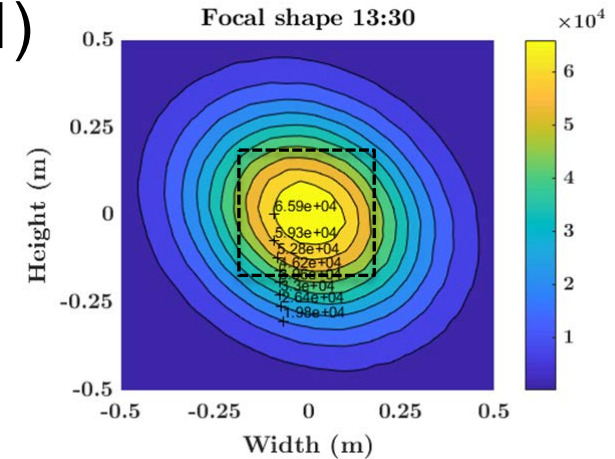
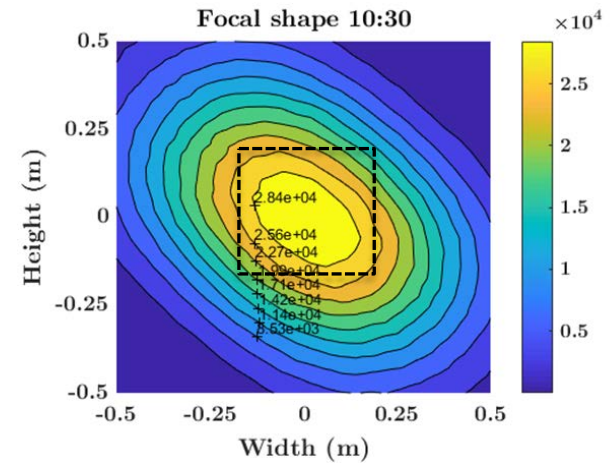


Figure 8: Heliostat field and test tower

Field Characterisation

Capability and limitations

- No data on field performance
- No means of measuring
- Large cosine losses (Eastern field)
- Limited window of opportunity



Results



Overall receiver thermal behaviour

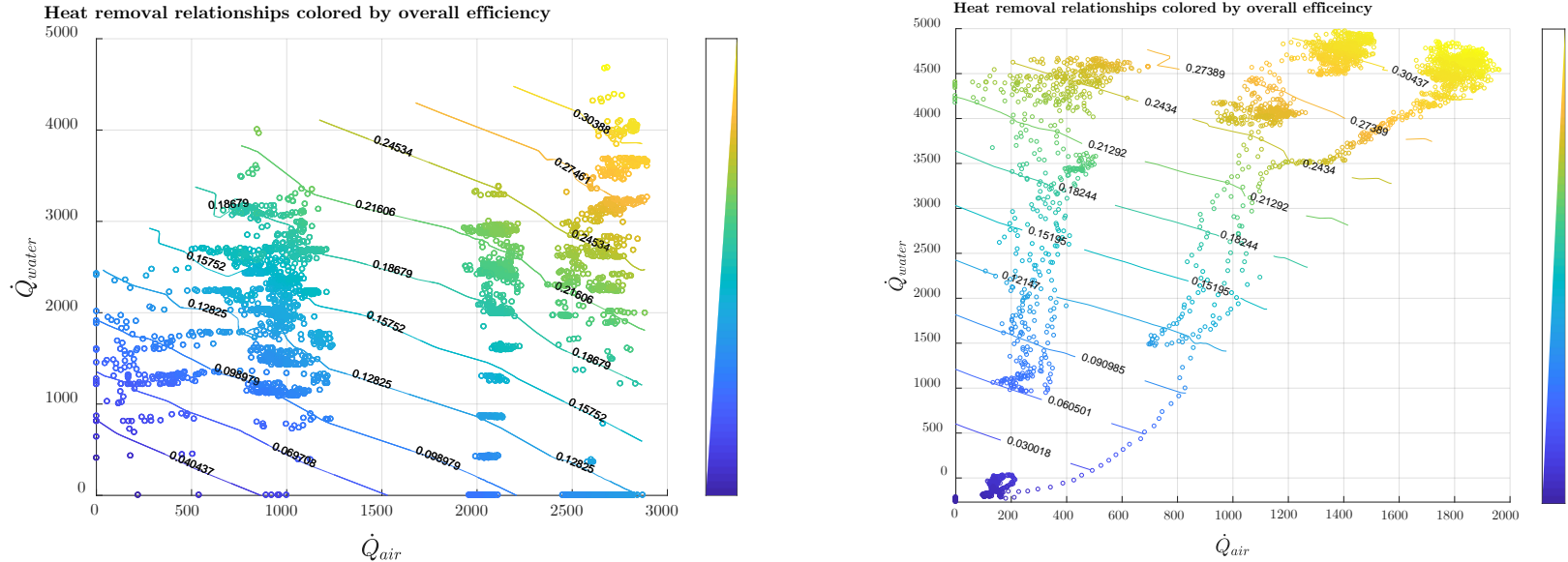


Figure 9: Overall field efficiency comparison for two tests

Results



Circumferential temperature distribution

- Fast ramp up after interruptions
- Control the thermal difference
- Location specific

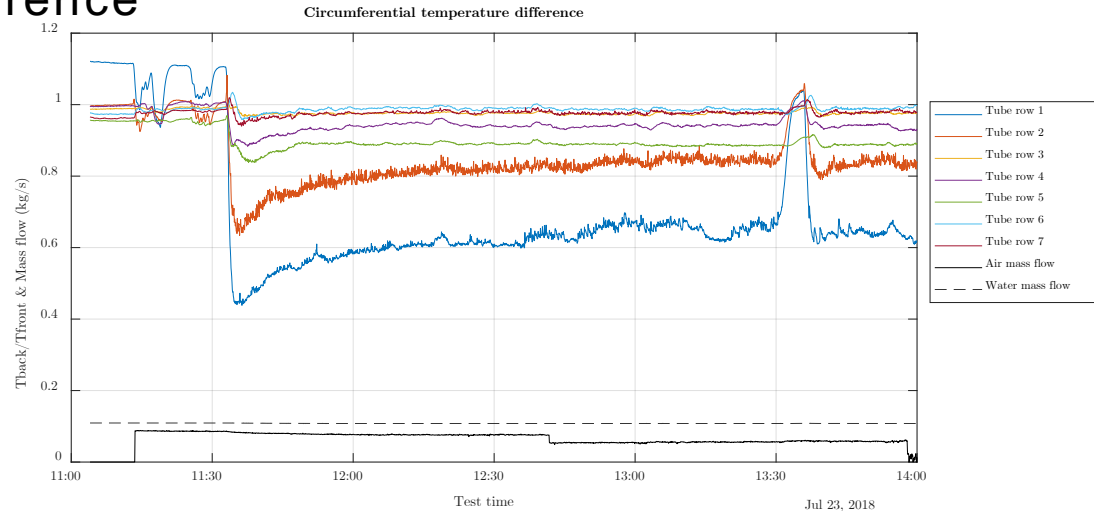


Figure 10: Sample response

Cavity temperature distribution

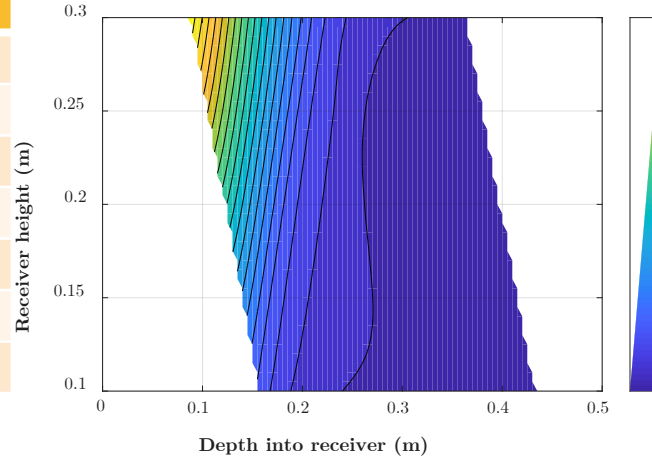


Interpolated steady-state distribution

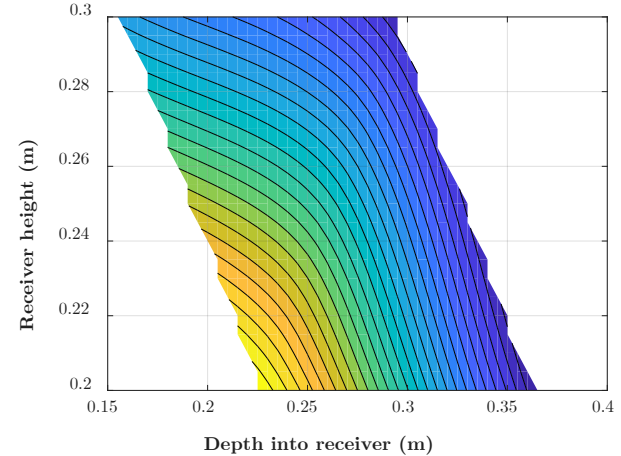
Table 1: Conditions at steady state

Variable	Value
DNI	855 W/m ²
T _{amb}	19.69°C
T _{water}	38.83°C
V _{wind}	0.69 m/s
\dot{m}_{air}	0.0713 kg/s
\dot{m}_{water}	0.0238 kg/s
V _{air in}	0.414 m/s

Interpolated temperature distribution on right wall



Interpolated temperature distribution on left wall



Sensitivities



Receiver response to environmental influences

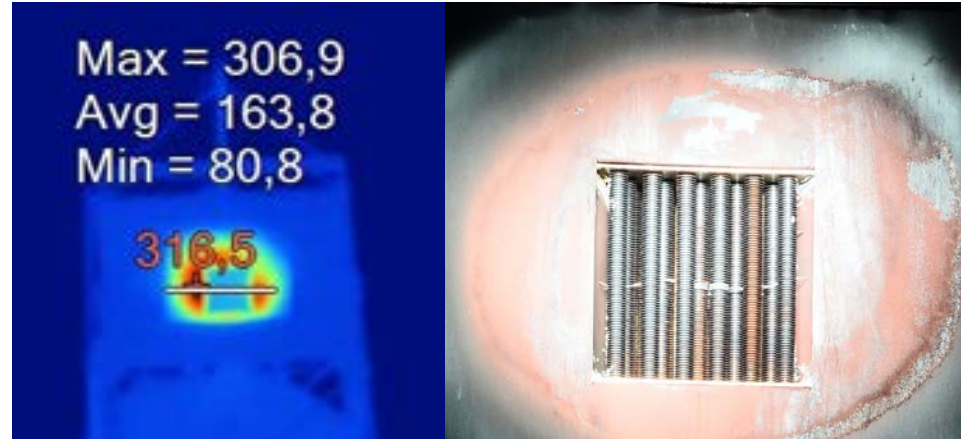
- Several variables influencing the tests
- Insensitive to ambient wind (max 7.3m/ s in test with aperture inlet velocity of 0.5m/ s)
- Mass flow rate relationship

Observations



Visual observations during the tests

- No volumetric effect
- No noticeable hot spot
- Spillage from field



Conclusion



The modified HPAR test demonstrated the following

- Ability to modulate the circumferential temperature gradient
- Ability to control the different energy absorption quantities
- Ability to capture/ repurpose convective losses

Thank you

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